



Comparison of linear and non-linear blade model predictions in Bladed to measurement data from GE 6MW wind turbine

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- Introduction
 - Non-linear blade model in Bladed
 - The turbine, environment and Bladed models

- Results
 - Power curve
 - Loads on blade, hub, tower

- Conclusions



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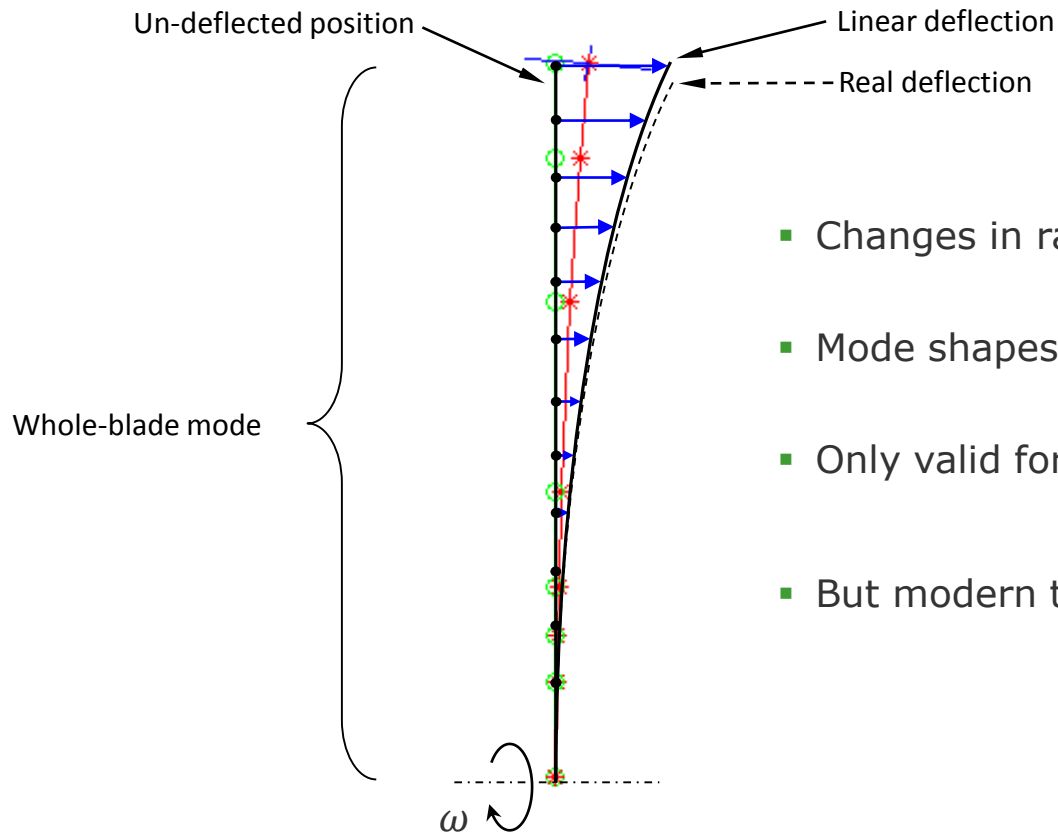
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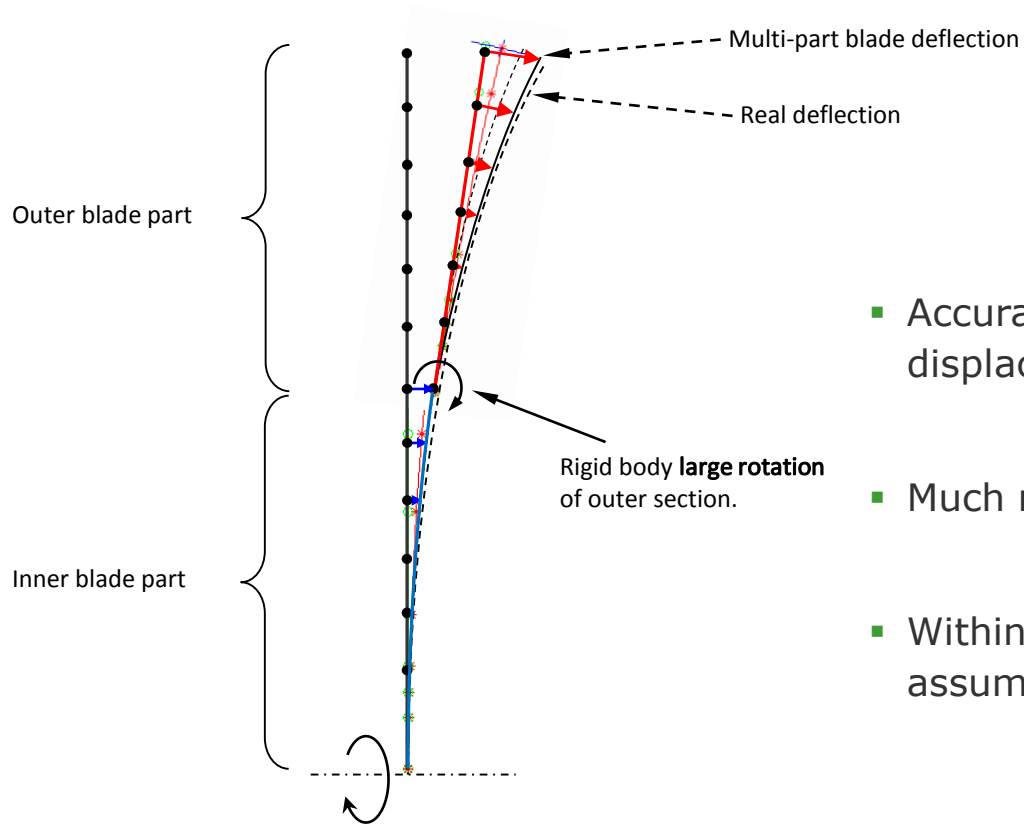
Linear blade model



- Changes in radial position not accounted for
- Mode shapes only correct for the undeflected blade
- Only valid for small deflections
- But modern turbine blades have large deflections!

Multi-part blade

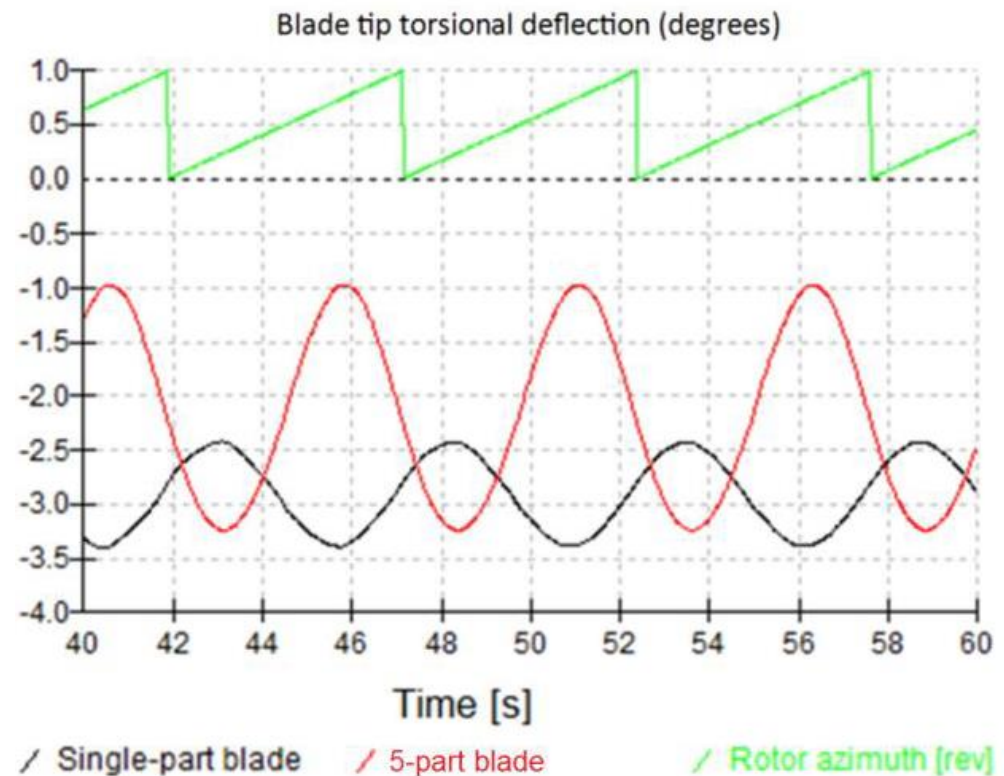
- Blade is several modal bodies



- Accurate model of large (non-linear) displacement, including radial displacement
- Much more accurate torsion prediction
- Within each blade part, small deflection assumption remains valid

The Bladed models

- Full turbine model defined by GE
- **Single-part blade**
 - 9 modes to include 1st torsional
- **Multi-part blade**
 - 5 blade parts, each with 8 modes



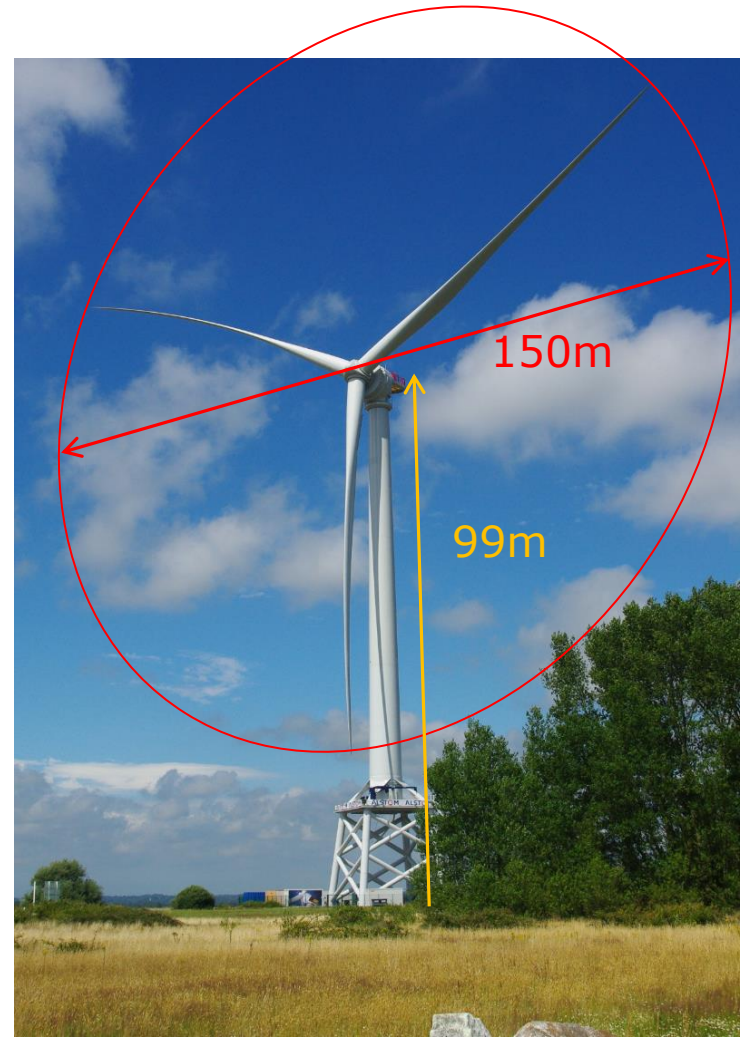
Aim of study

- **Aim**
 - Compare “single-part” and “multi-part” blade model results to measurements from GE Haliade 6MW turbine
 - Power
 - Loads
 - Blade deflection



The turbine

- GE Haliade 6MW (onshore prototype)
- LM blade 73.5m
- Direct drive



The environment

- Data collection
 - Wind speed and TI measured near turbine (2D away)
 - Wind speed 5-15m/s and filtered for TI = 10-12%
 - Wind shear and air density measured for each wind bin
 - Strain gauges at blade root, main shaft, tower base
 - Blade deflection measured with ground-based laser

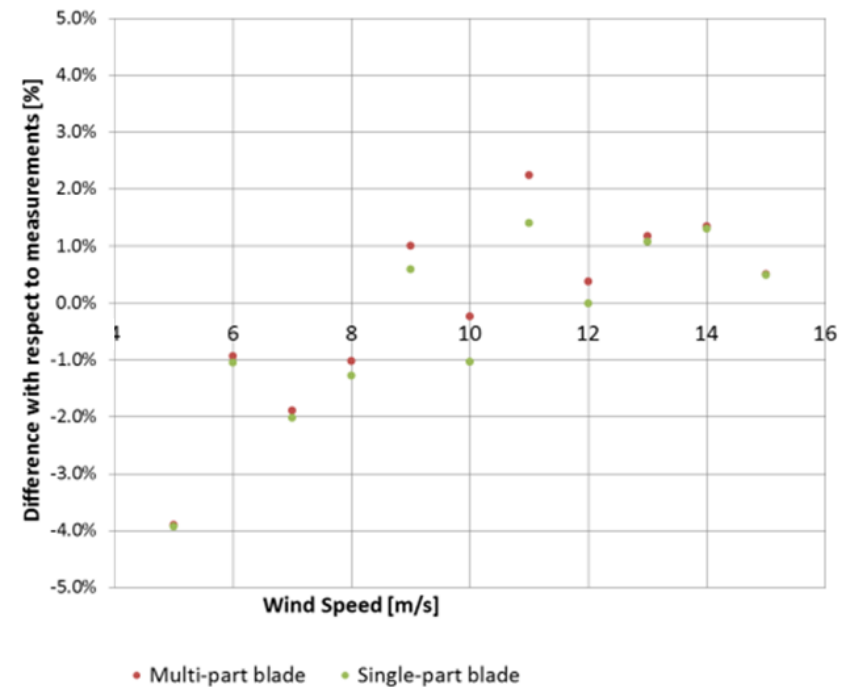
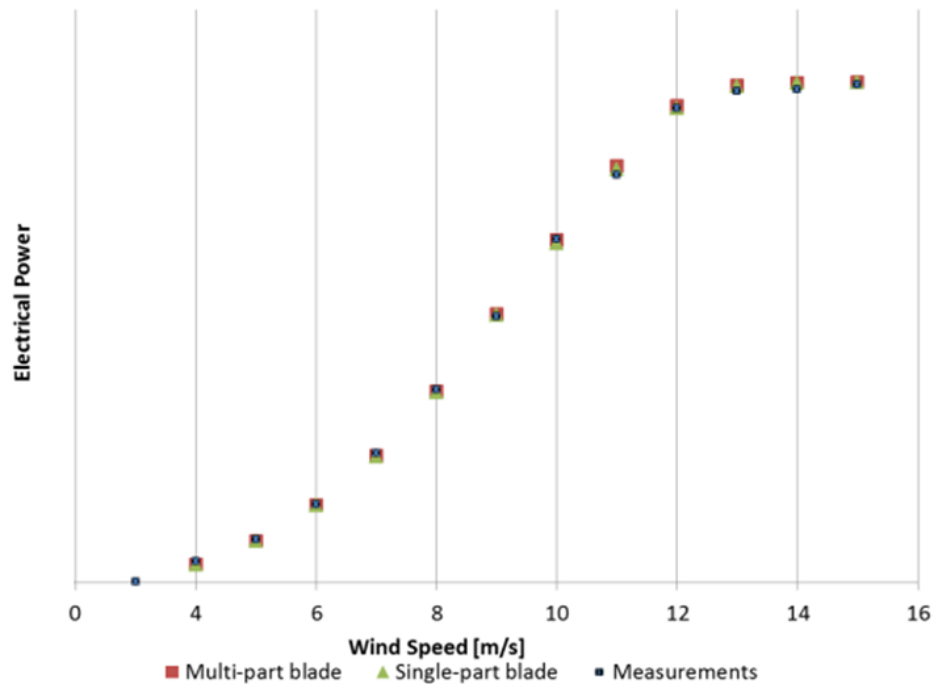
- Bladed wind inputs
 - Measured speed, shear and air density
 - Kaimal turbulence TI = 11%
 - Upflow = 0°
 - 6 turbulence seeds (yaw -8, 0, 8)

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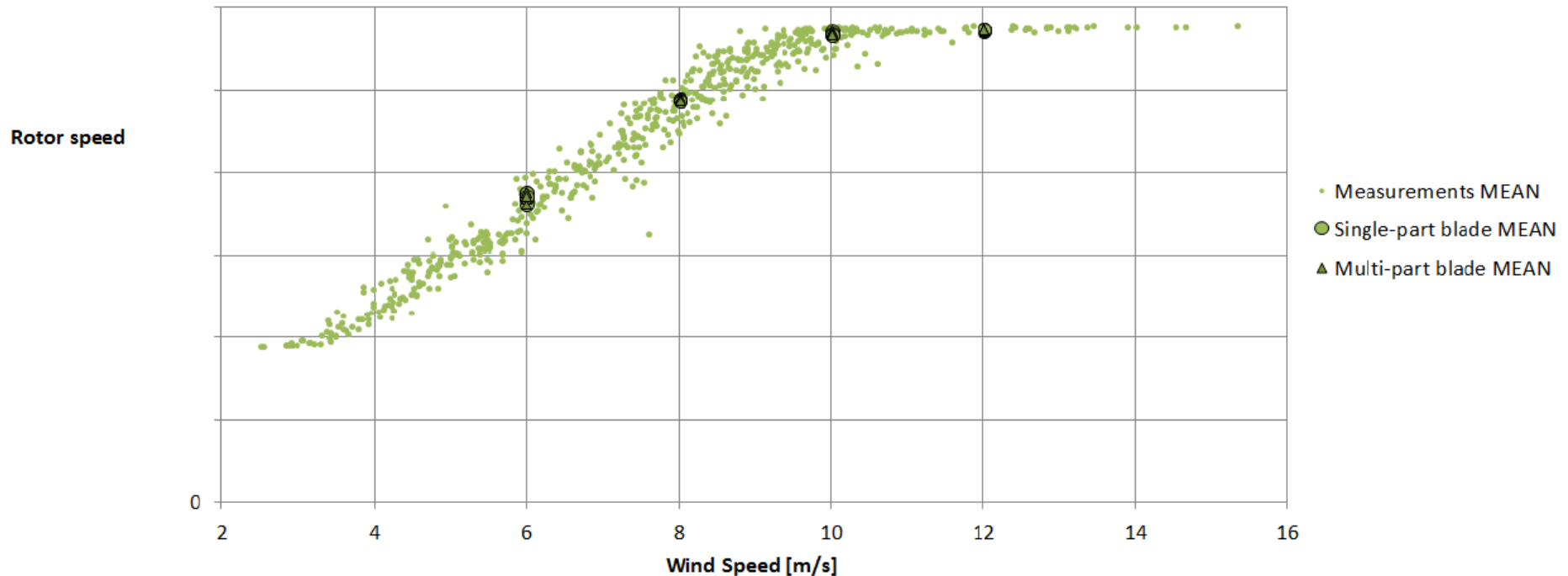
Results – power curve

- Electrical power prediction relative to measurements – generally within 2%



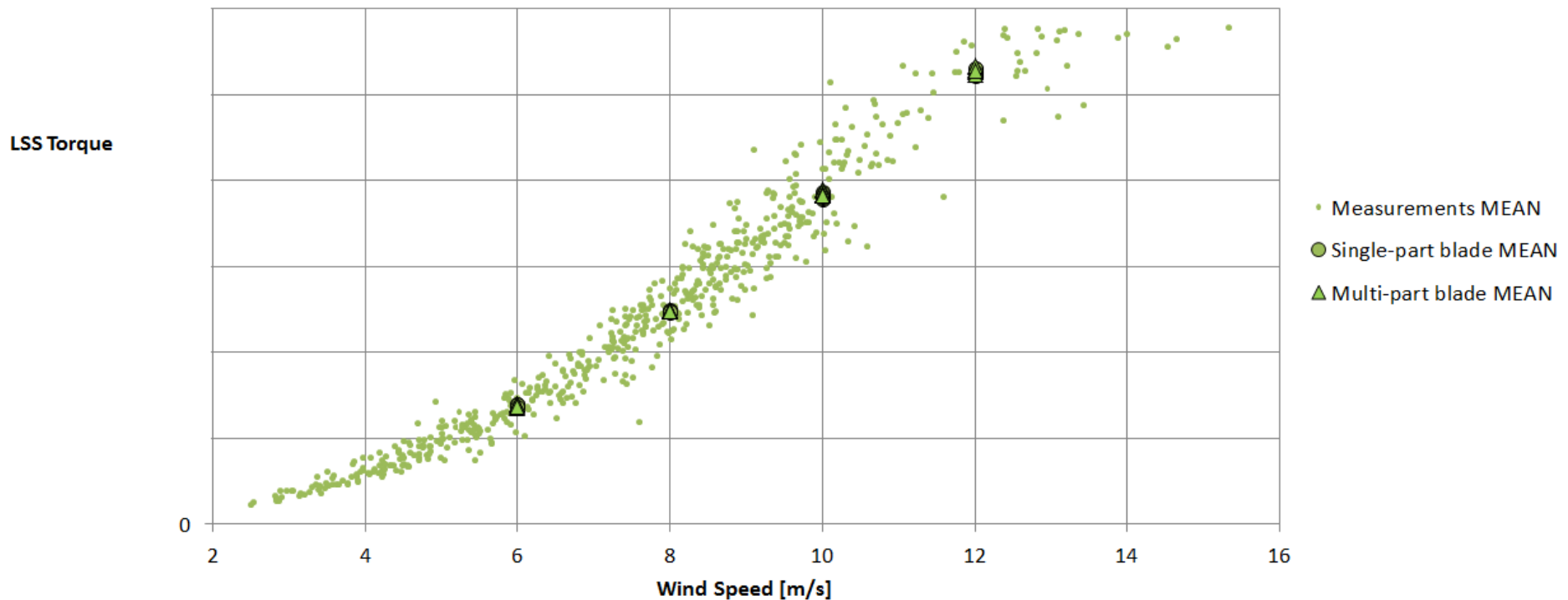
Results – loads (operating point)

- Check match in operating point
- Rotor speed mean values match well



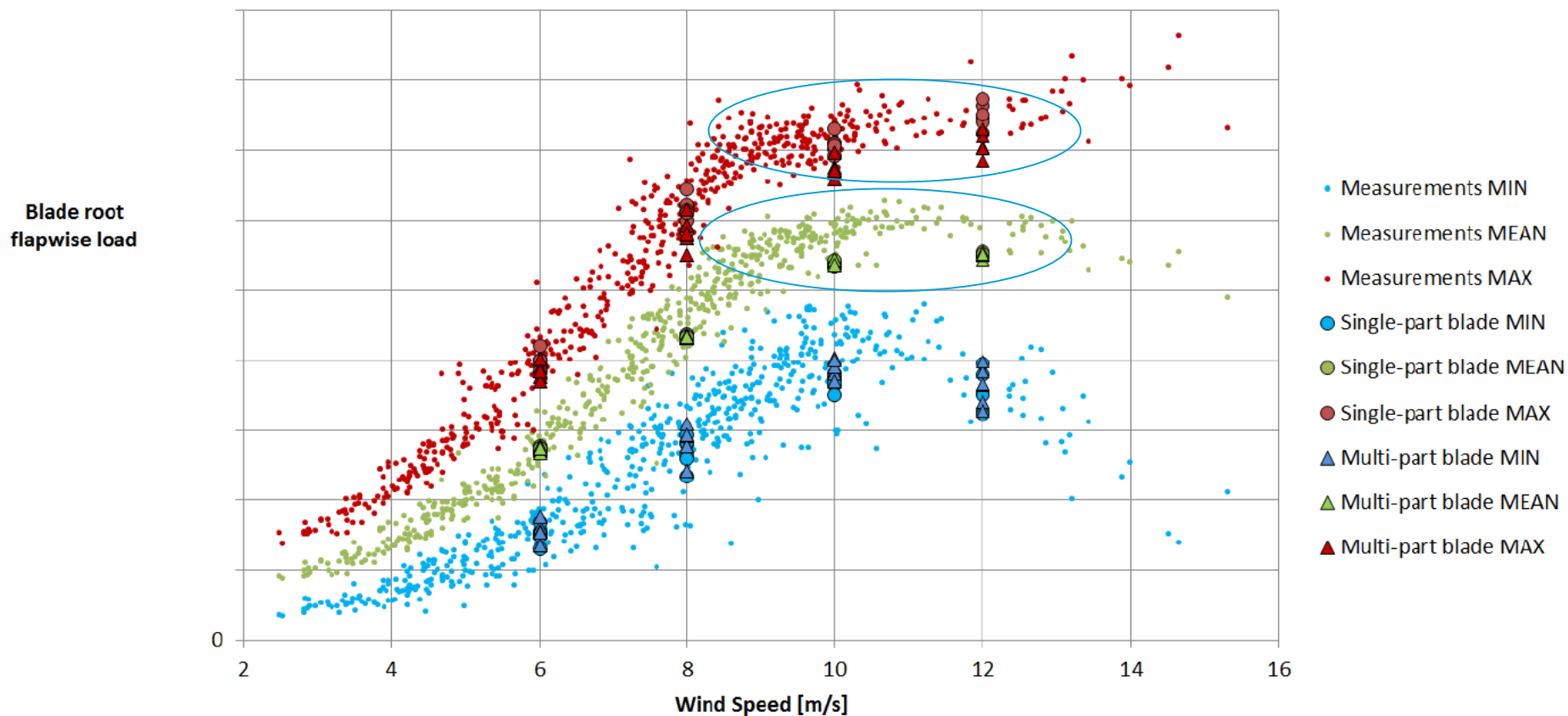
Results – loads (operating point)

- Check match in operating point
- Shaft torque mean values match well



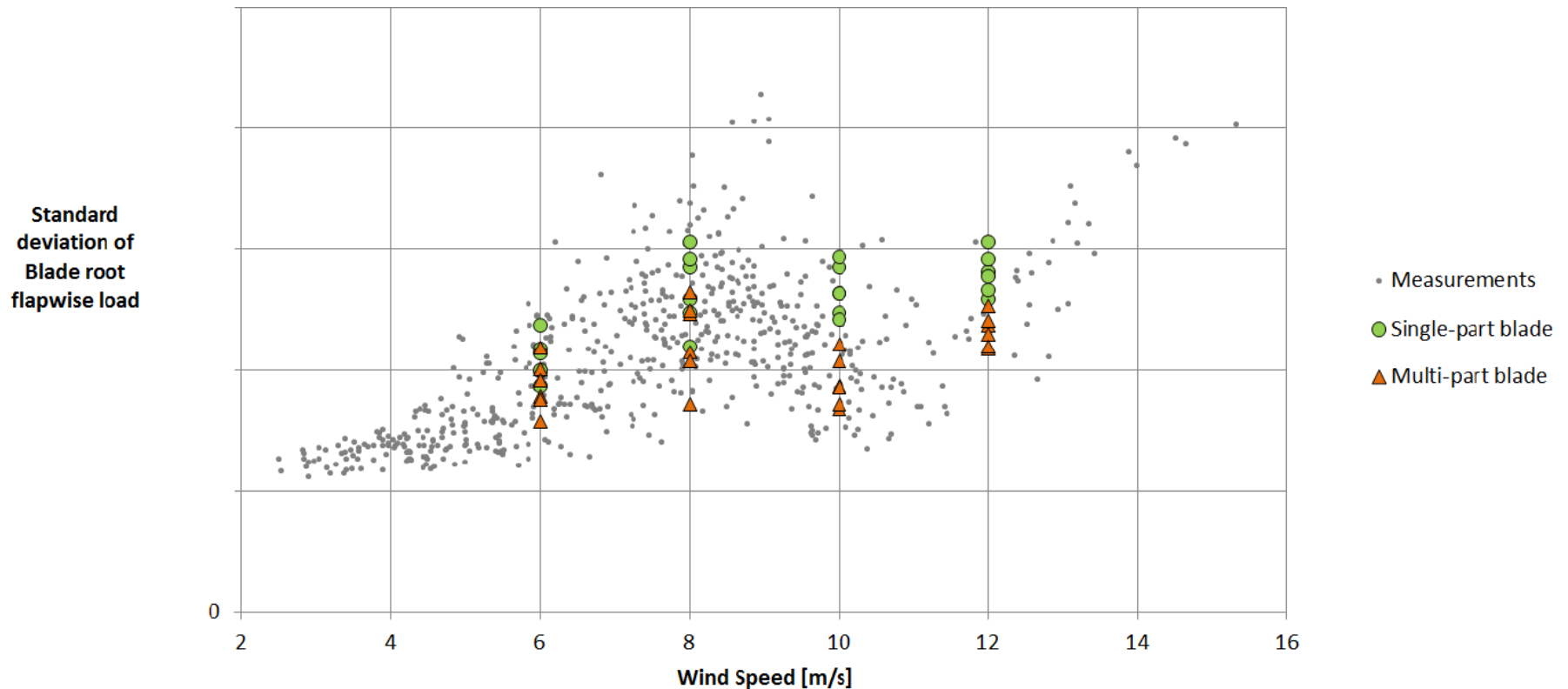
Results – blade flapwise loads

- Blade flapwise loads **Min, Mean, Max**
 - Offset in mean value between simulation and measurements



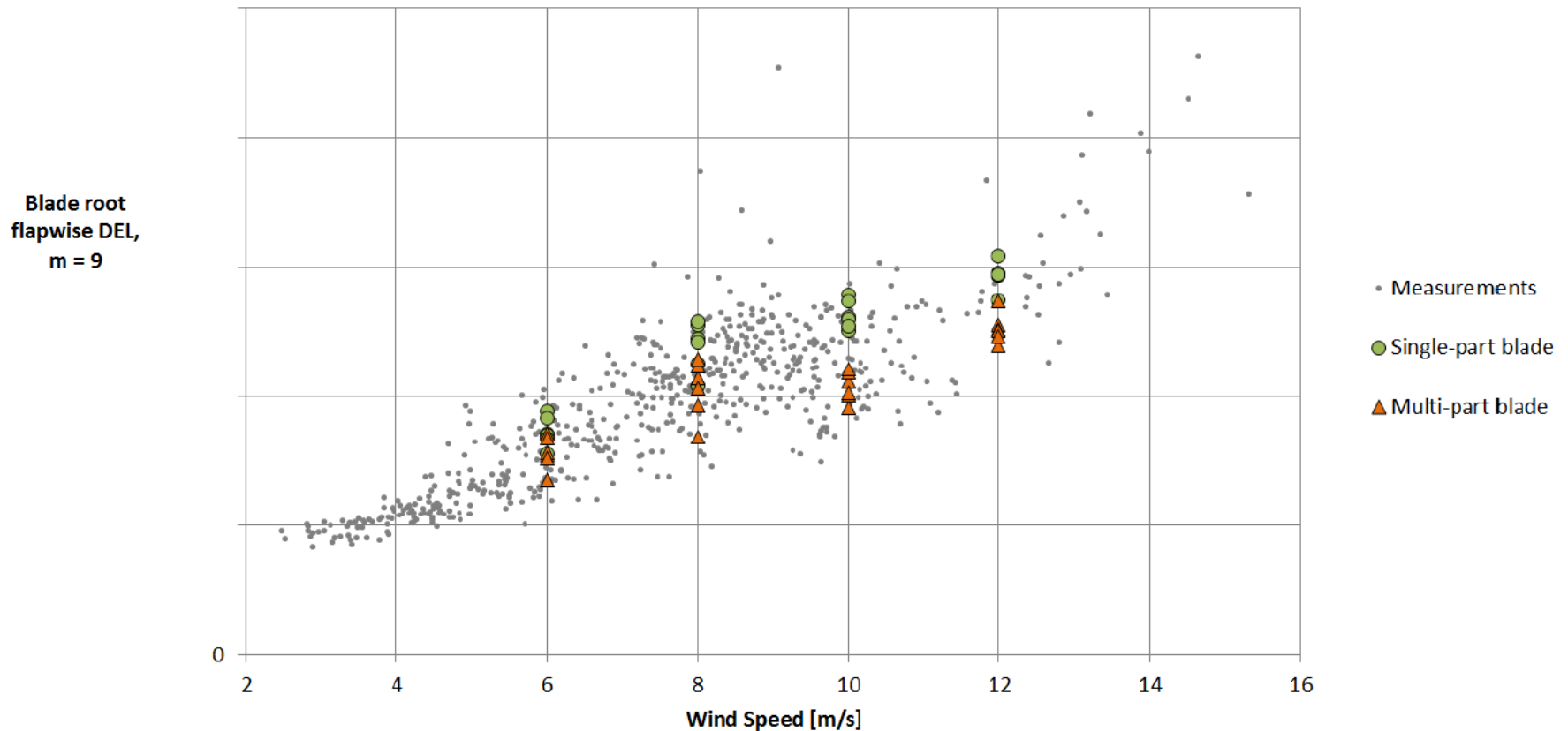
Results – blade flapwise loads

- Blade flapwise loads **standard deviation**
 - Good match suggesting range is well captured



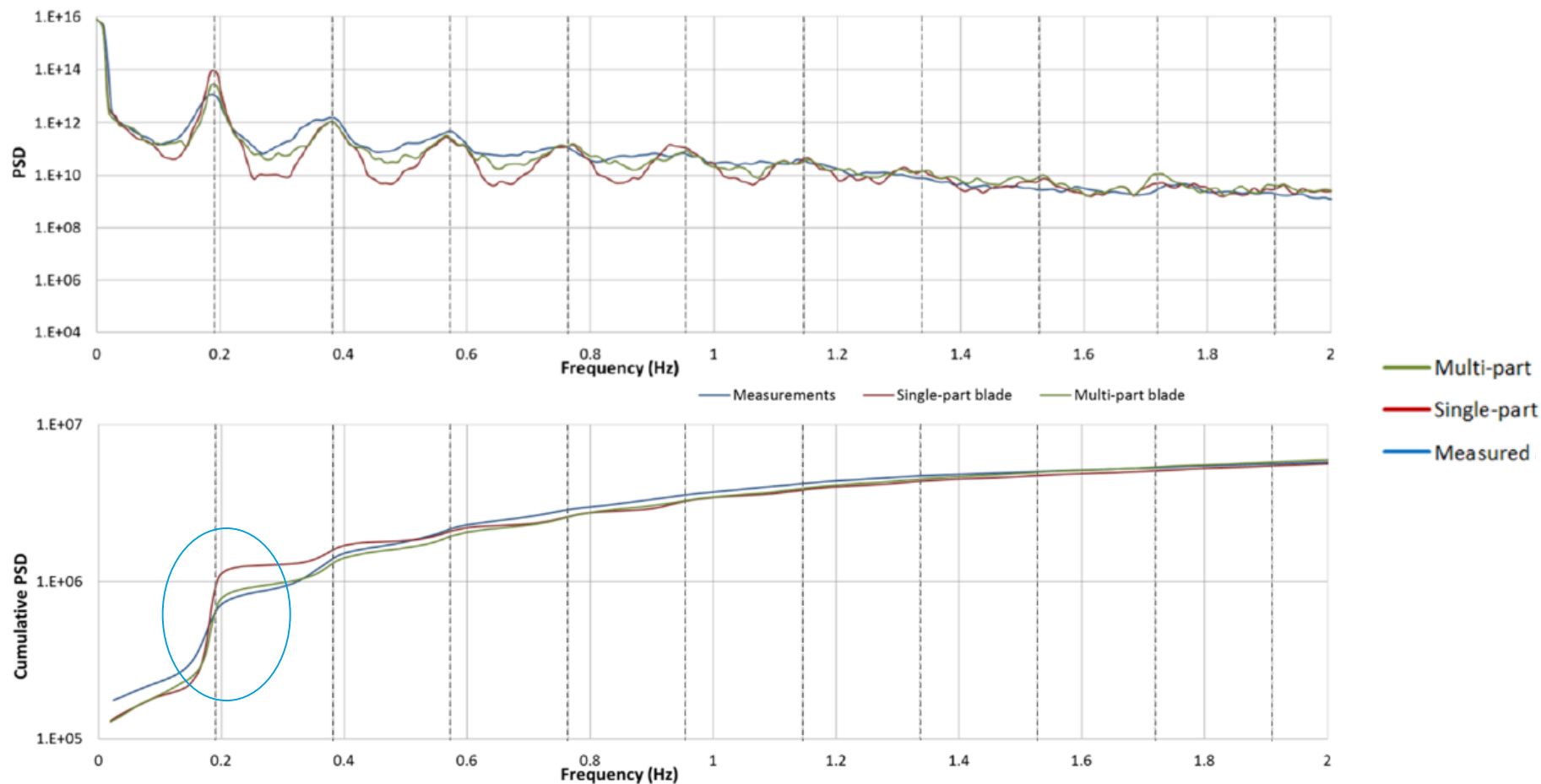
Results – blade flapwise loads

- Blade flapwise loads **DEL**
 - Multi-part centred in cloud of measurements. Single-part near top.



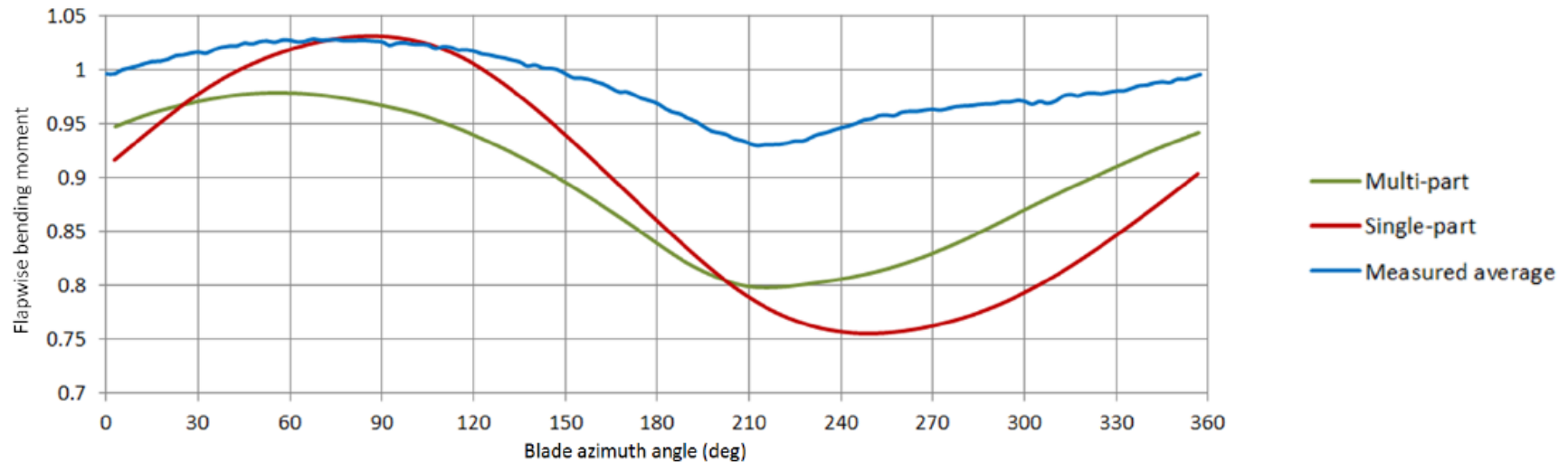
Results – blade flapwise loads

- Blade flapwise loads **PSD** – main difference at 1p



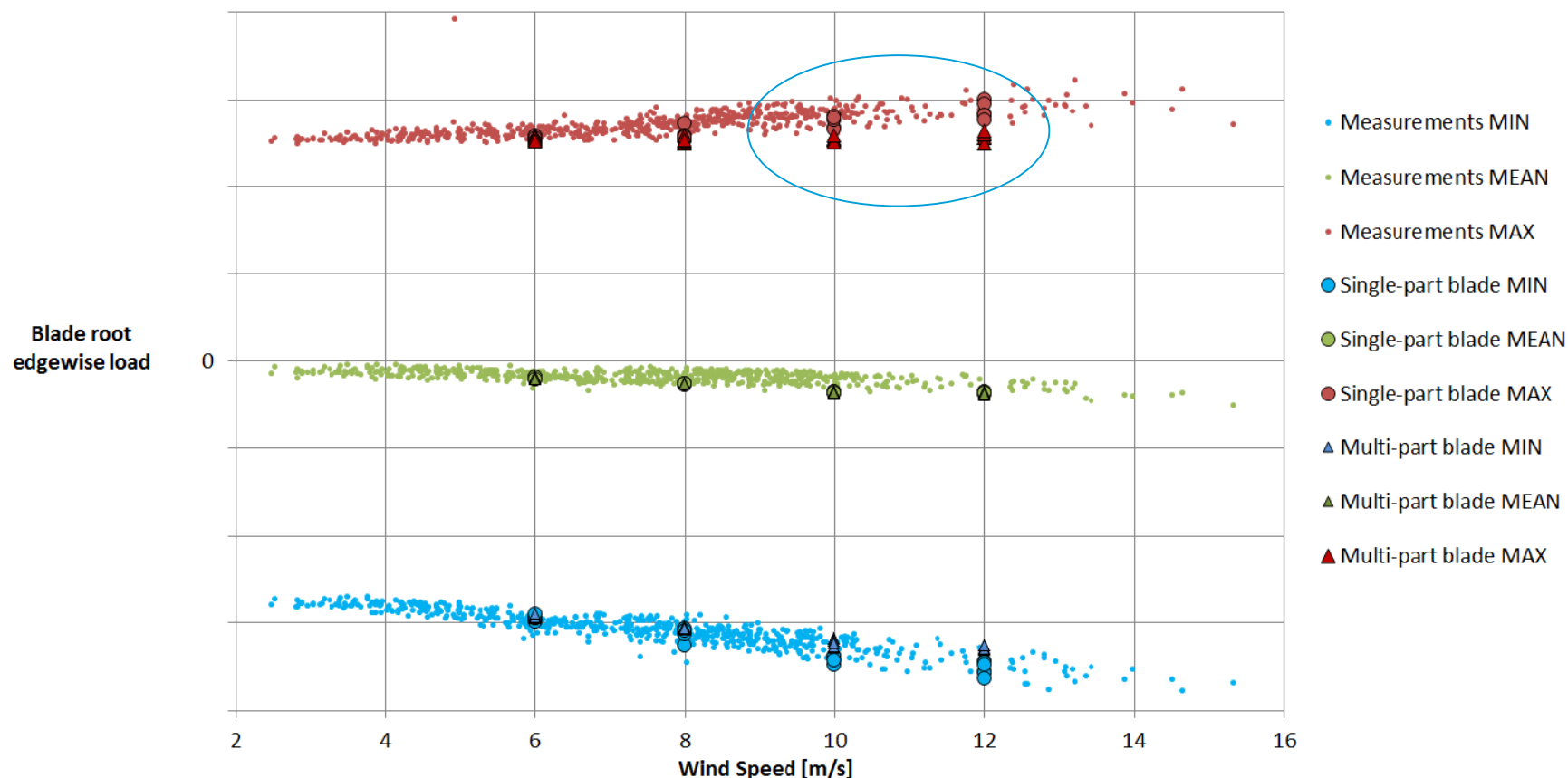
Results – blade flapwise loads

- Blade flapwise load **periodic component**
 - Multi-part matches better in phase and amplitude



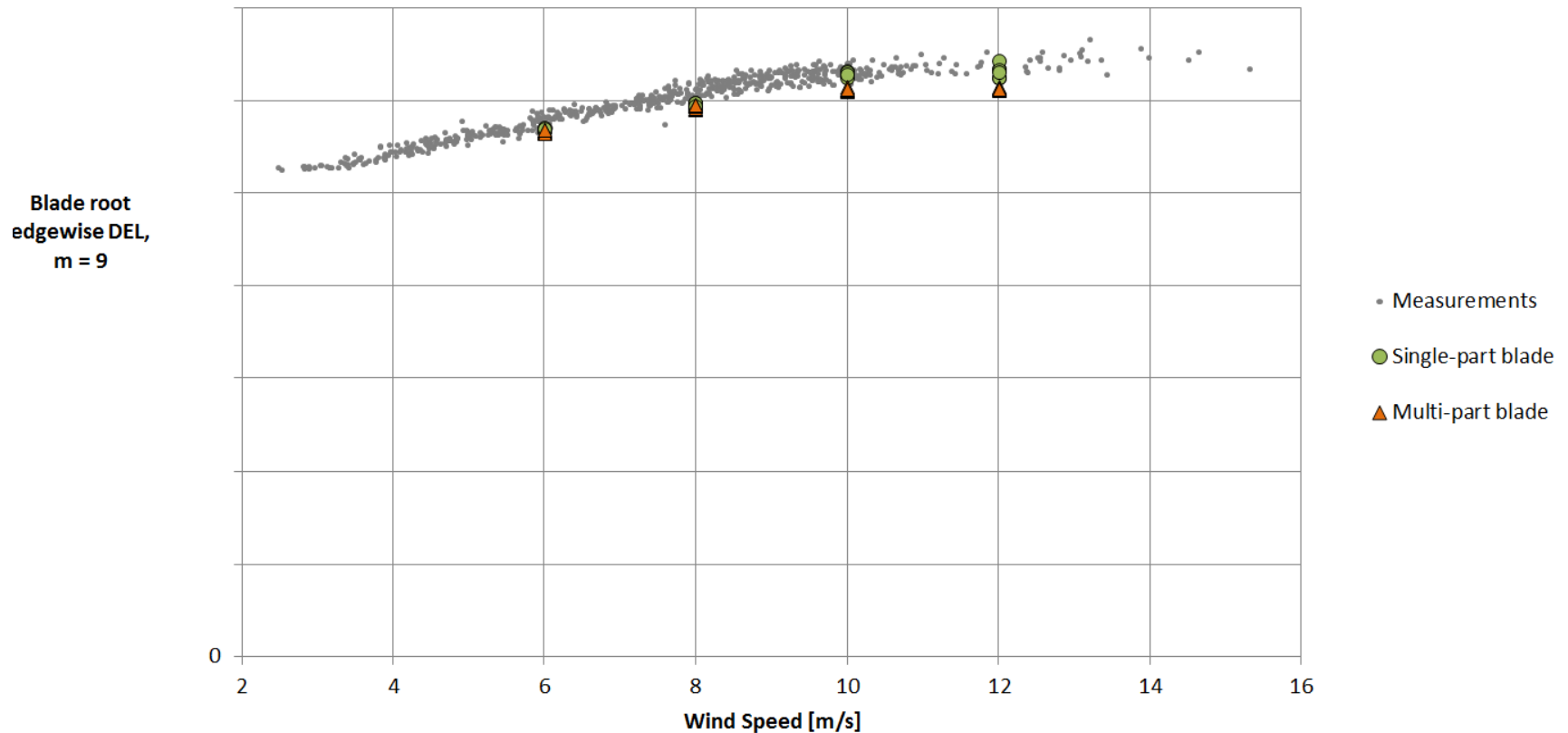
Results – blade edgewise loads

- Blade edgewise loads **Min, Mean, Max**
 - Good match generally. Single-part matches max loads better



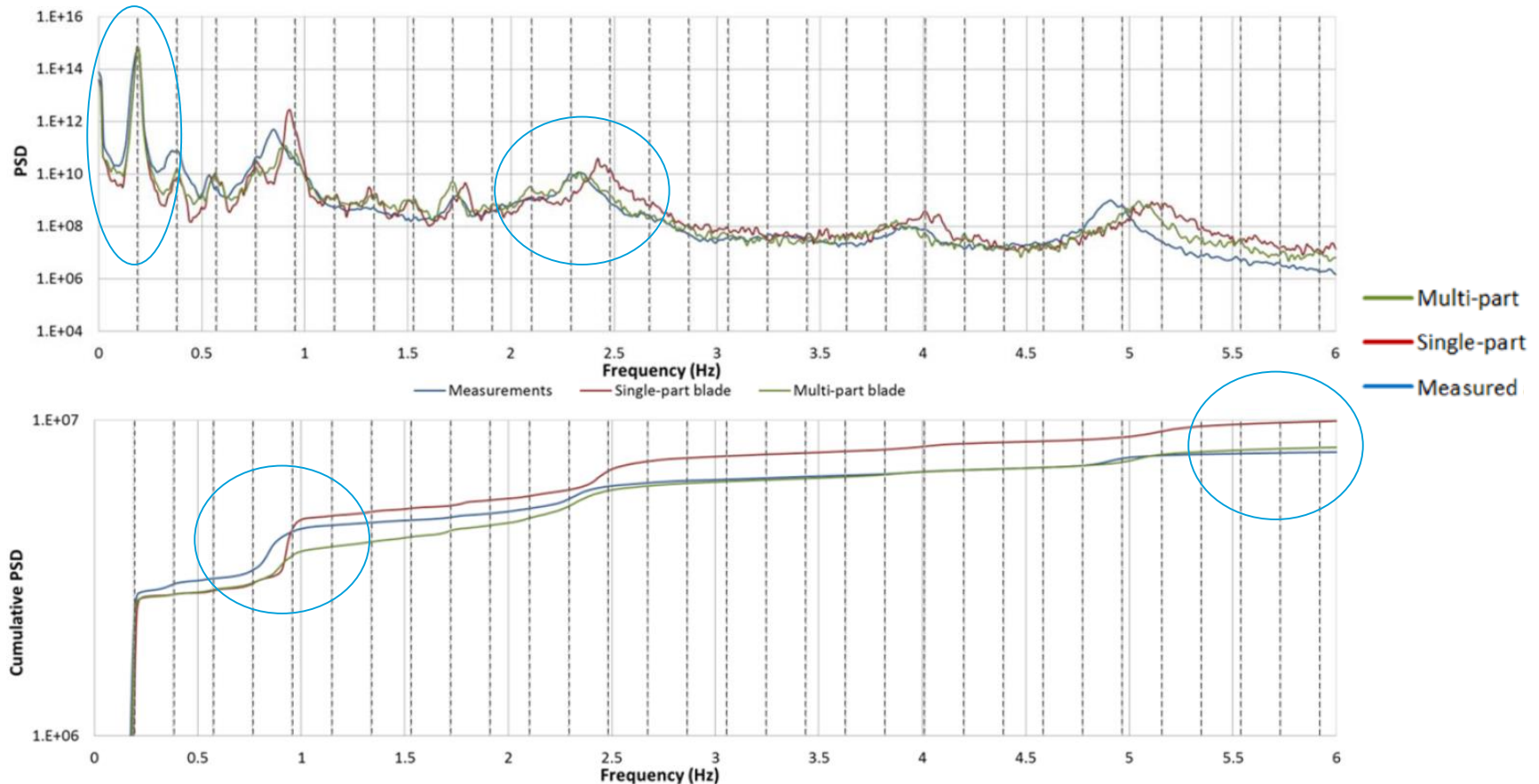
Results – blade edgewise loads

- Blade edgewise loads **DEL**
 - Single-part slightly closer to measurements



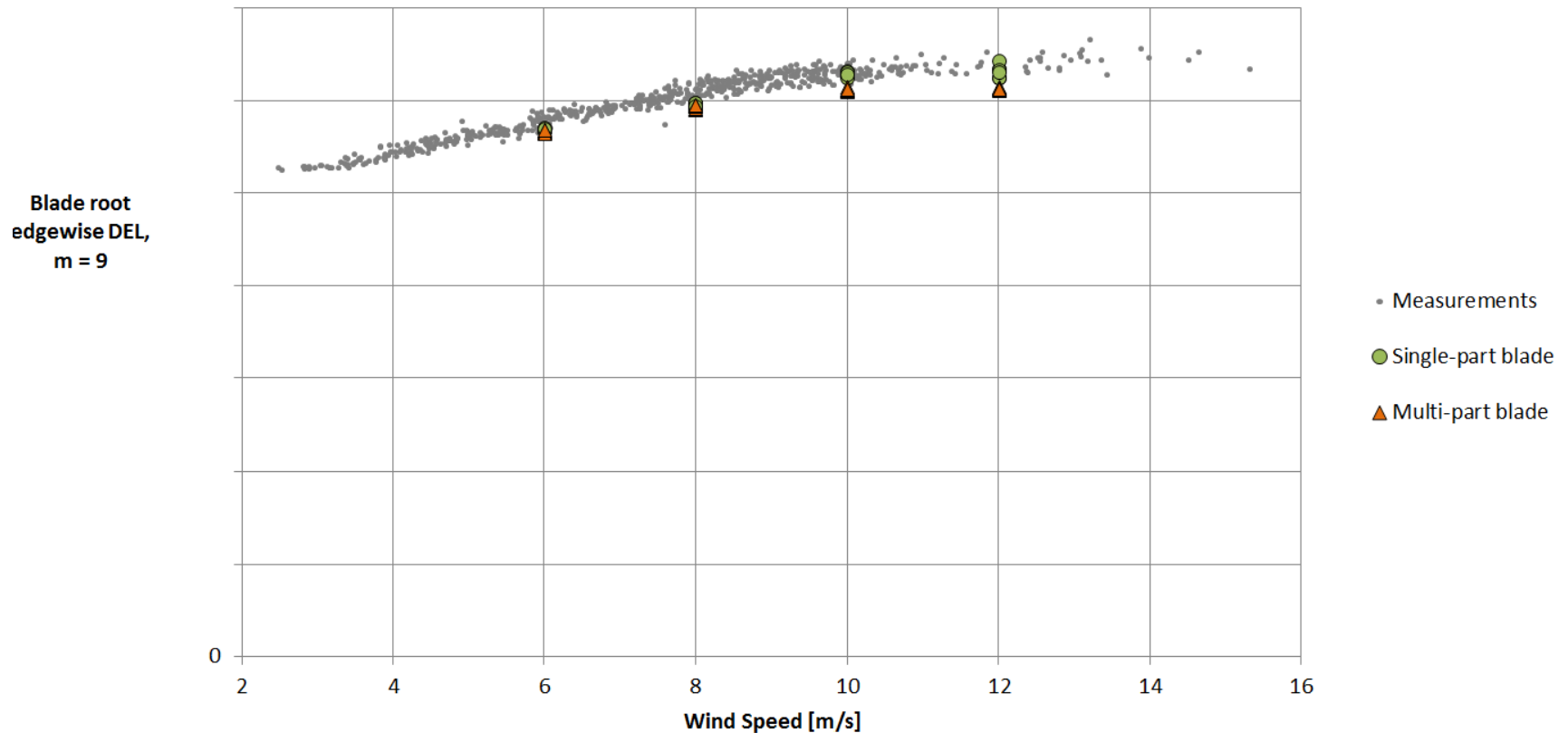
Results – blade edgewise loads

- Blade edgewise loads **PSD**
 - Multi-part dynamic response looks better (contradicts DELs)



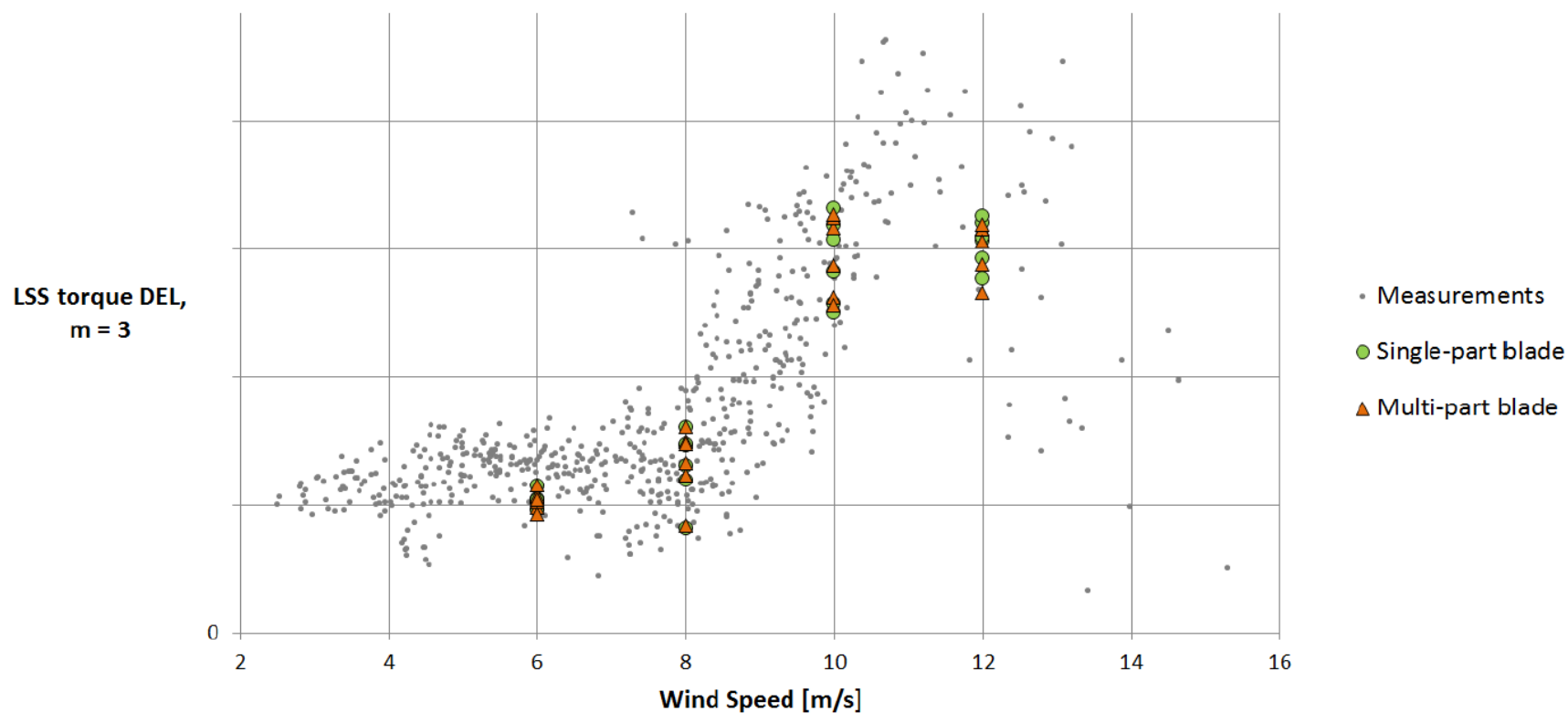
Results – blade edgewise loads

- Blade edgewise loads **DEL**
 - Single-part slightly closer to measurements



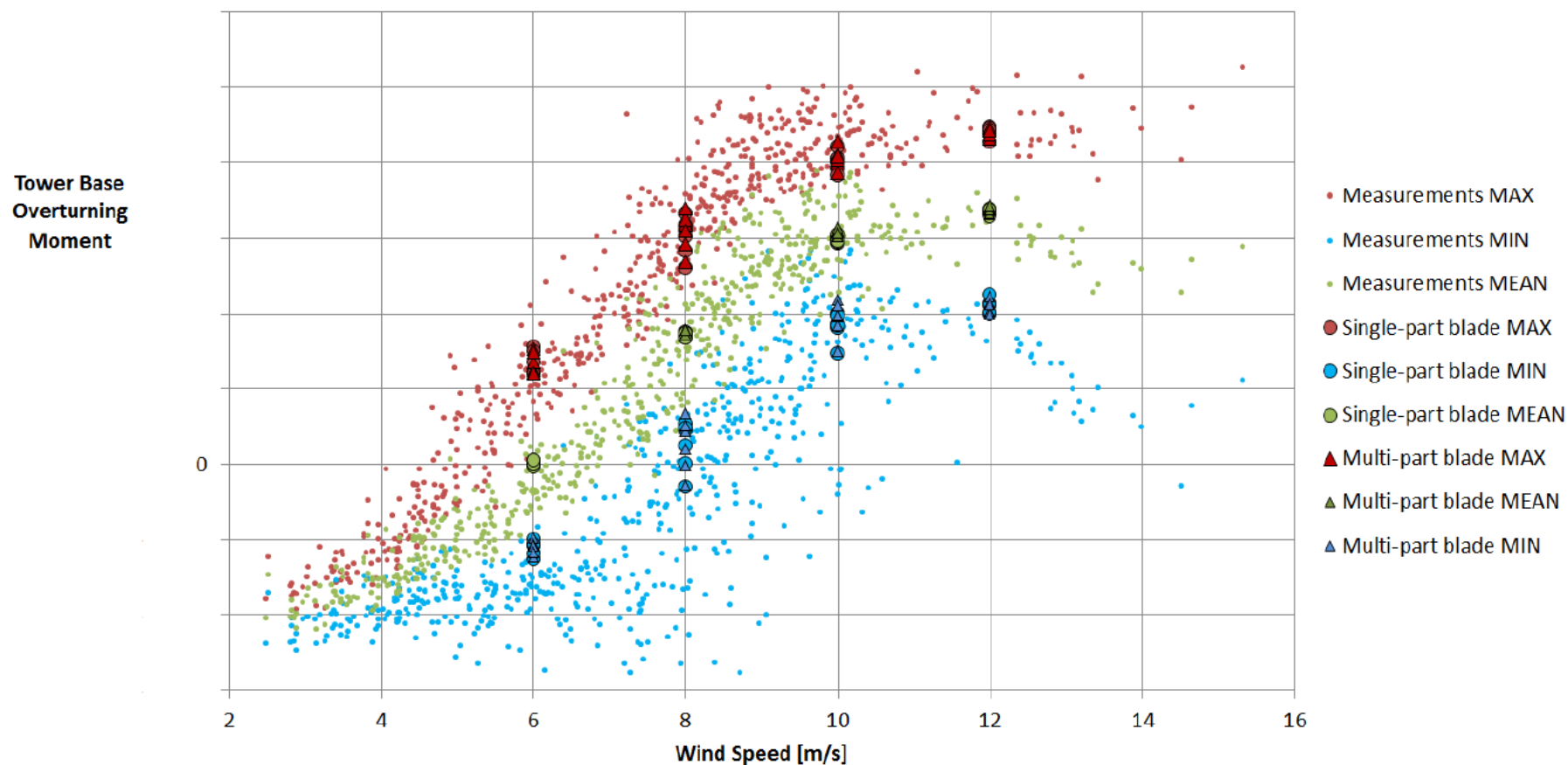
Results – shaft torque loads

- Good match in LSS **DELs**



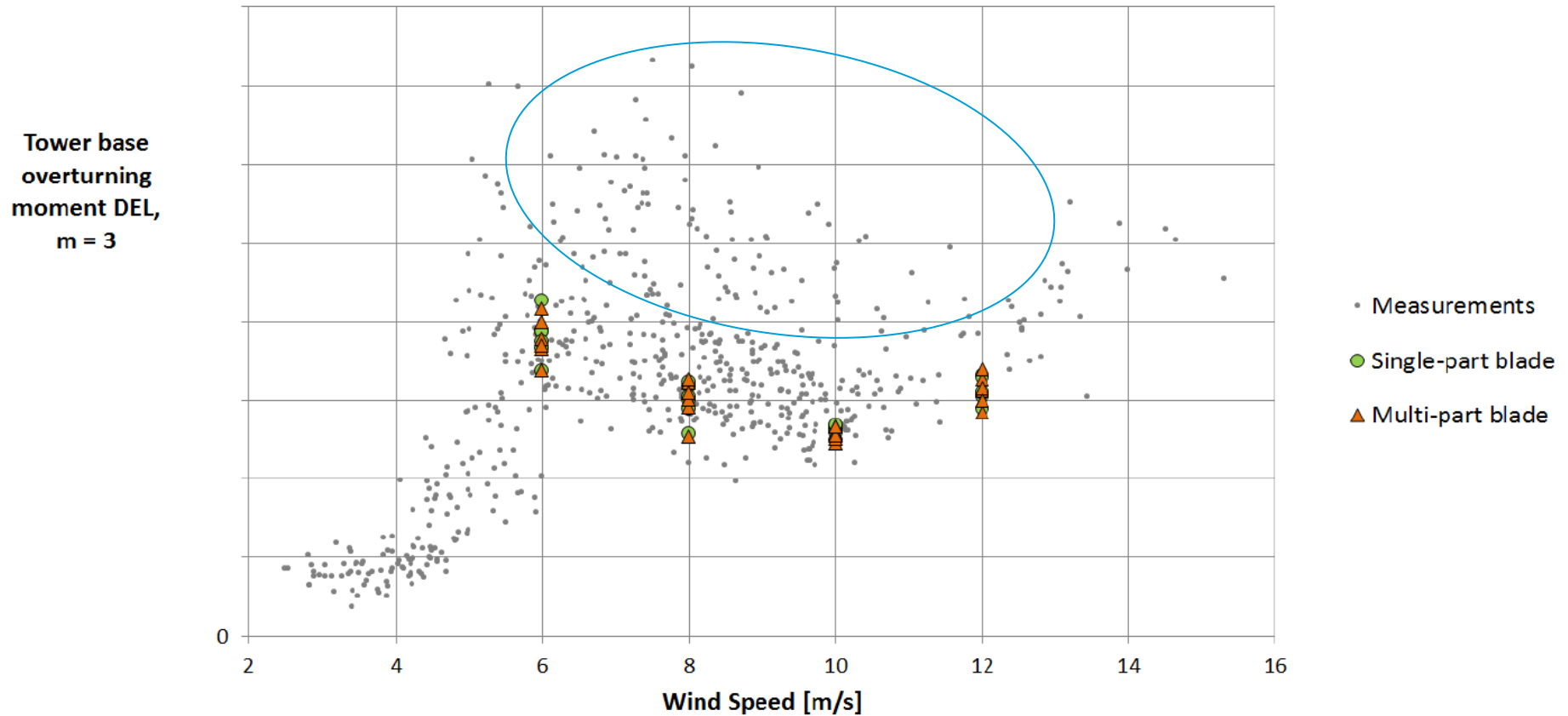
Results – tower base loads

- Good match in tower **Min, Mean, Max**



Results – tower base loads

- Ok match in tower **DELs** – not capturing highest values



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Conclusions

- Single-part and multi-part both generally show a good match to measurement power, loads and blade deflection
- Measured power generally within 2% of simulated
- Blade flapwise loads matched better to measurements with multi-part
 - periodic load is a contributor to differences
- Blade edgewise DELs closer to measurements for single-part
 - dynamic response of multi-part looks better
 - other factors? (Aerodynamics, wind inflow conditions etc.)

